

# The pulsating brain: an interface-coupled fluid-poroelastic model of the cranial cavity

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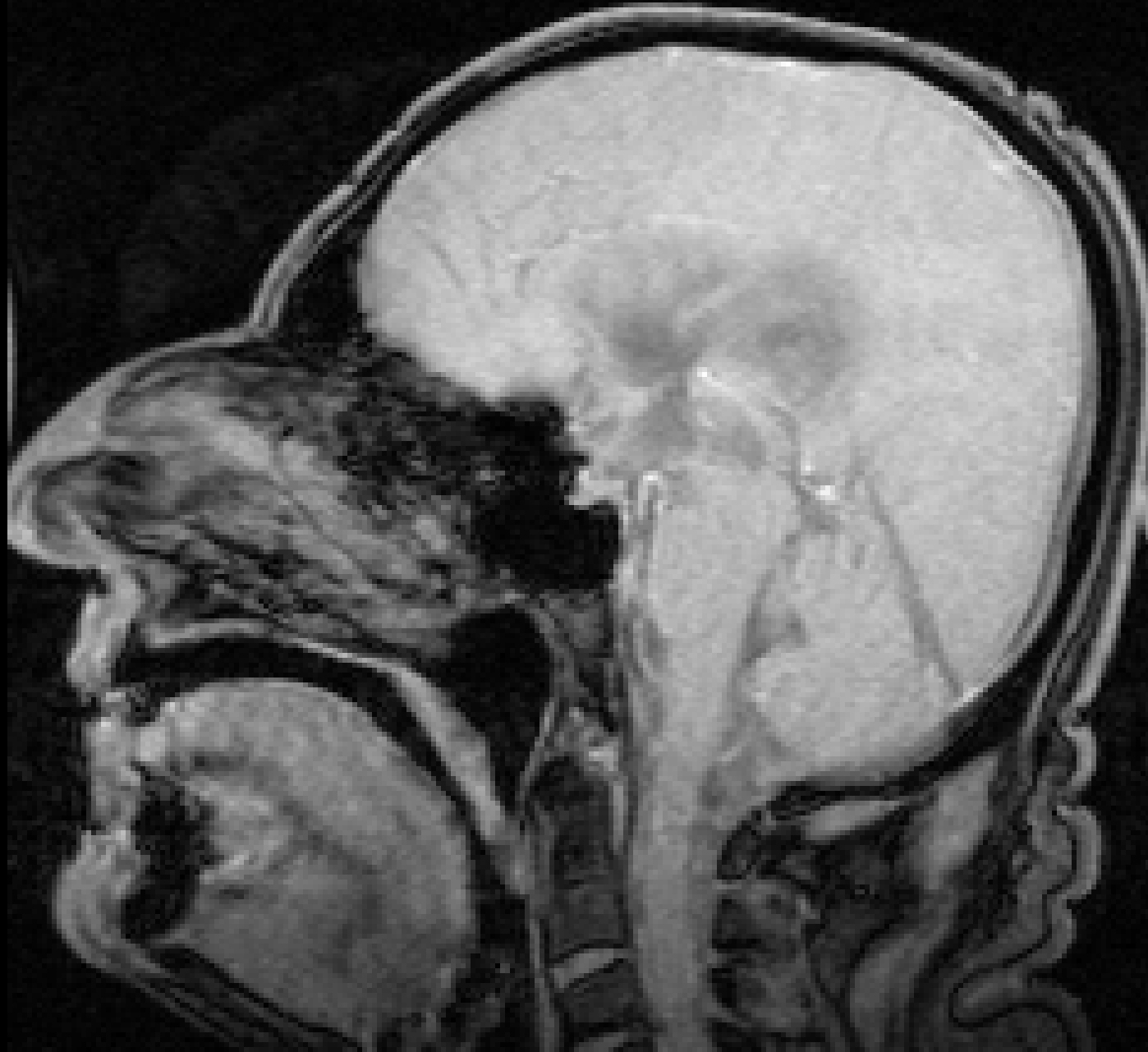
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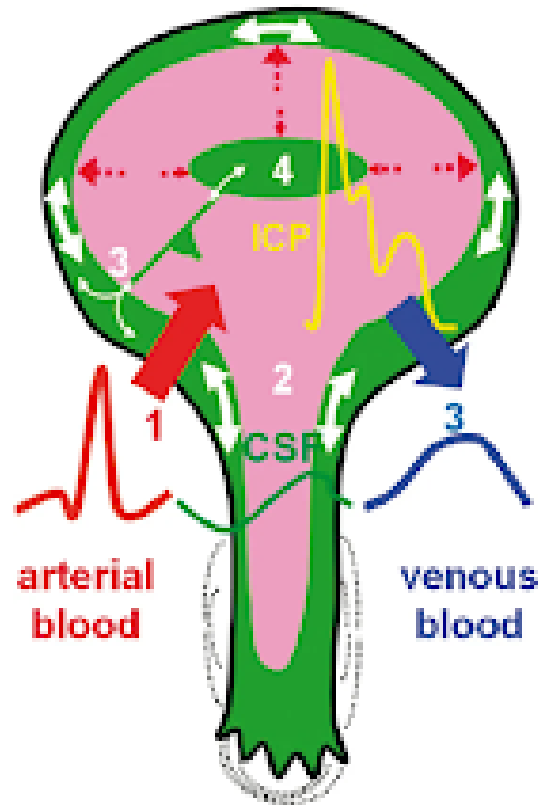
**simula**



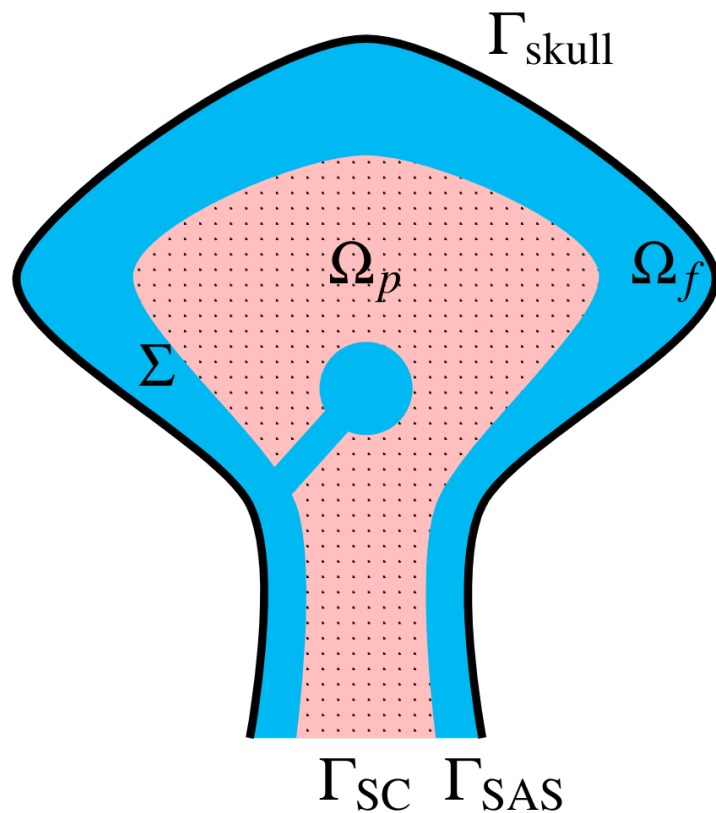
**Cardiac  
pulsations drive  
oscillatory  
motion in the  
cranial cavity**

[Nevit Dilmen, NPH patient,  
Wikimedia Commons, 2010 ]

# The disbalance of arterial inflow and venous outflow drives pressure pulsations and CSF flow



# A computational framework for intracranial pulsatility



a) **Stokes flow** - CSF-filled spaces -  $\Omega_f$

$$\rho_F \partial_t \mathbf{u} - \operatorname{div} [2\mu_F \boldsymbol{\epsilon}(\mathbf{u}) - p_F \mathbf{I}] = 0$$

$$\operatorname{div} \mathbf{u} = 0$$

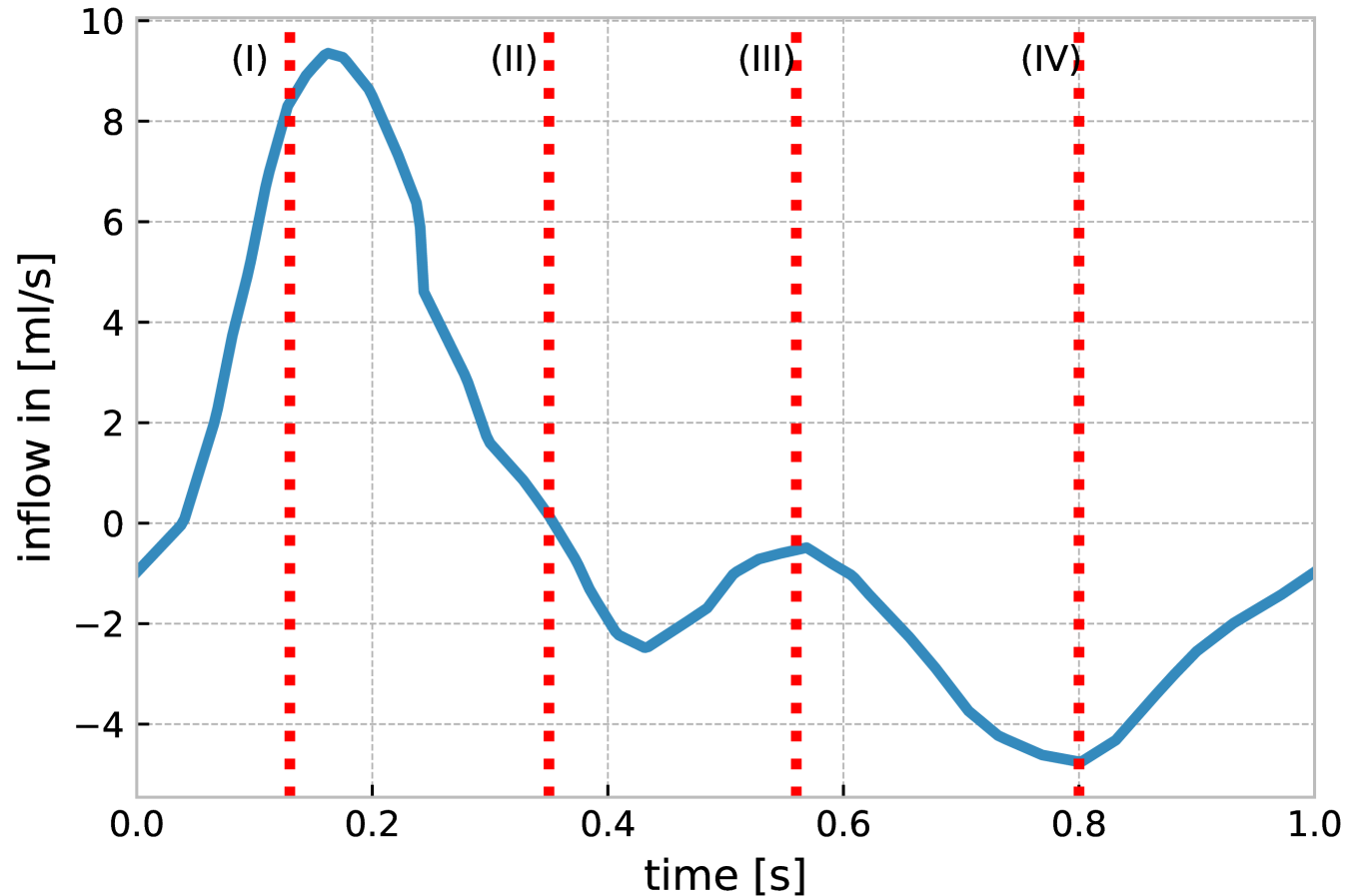
b) **Poroelasticity (Biot)** - brain tissue -  $\Omega_p$

$$-\operatorname{div} [2\mu_S \boldsymbol{\epsilon}(\mathbf{d}) + \lambda \operatorname{div} \mathbf{d} - \alpha p_p \mathbf{I}] = 0$$

$$c_0 \partial_t p_p - \alpha \partial_t \operatorname{div} \mathbf{d} + \operatorname{div} \left( \frac{\kappa}{\mu_F} \nabla p_p \right) = g$$

c) **Interface conditions** on  $\Sigma$

# The disbalance of arterial inflow and venous outflow drives intracranial pulsatile motion



(I) early systole - high net blood inflow

(II) end of net blood inflow

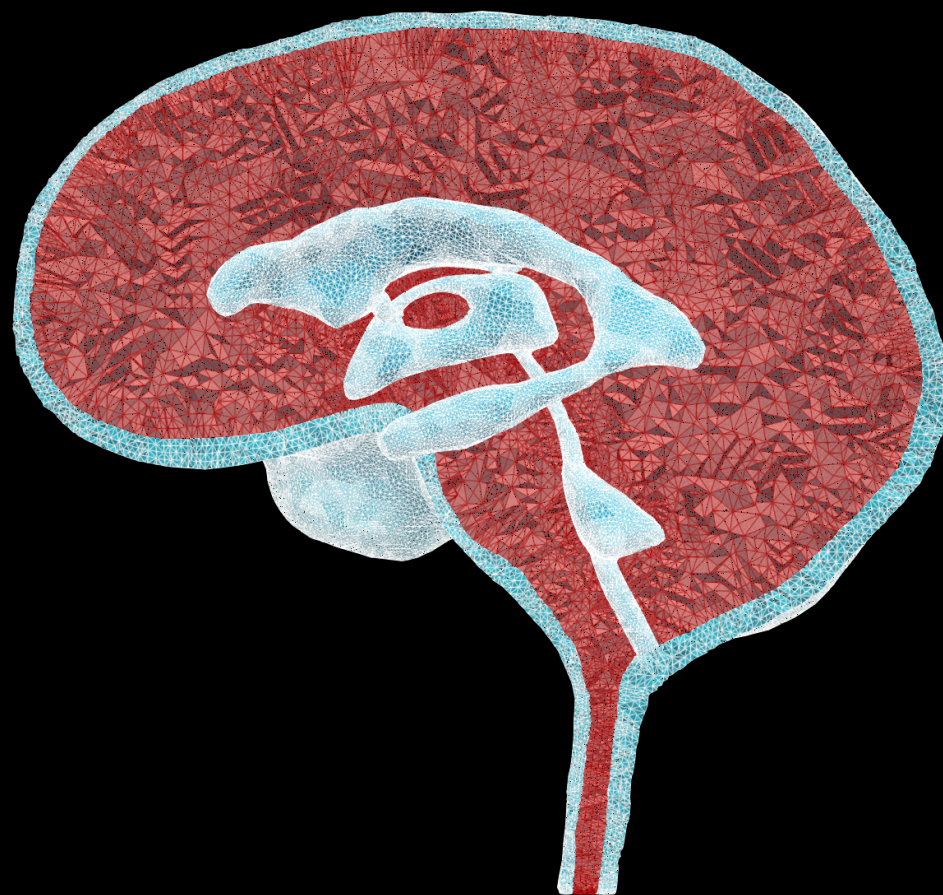
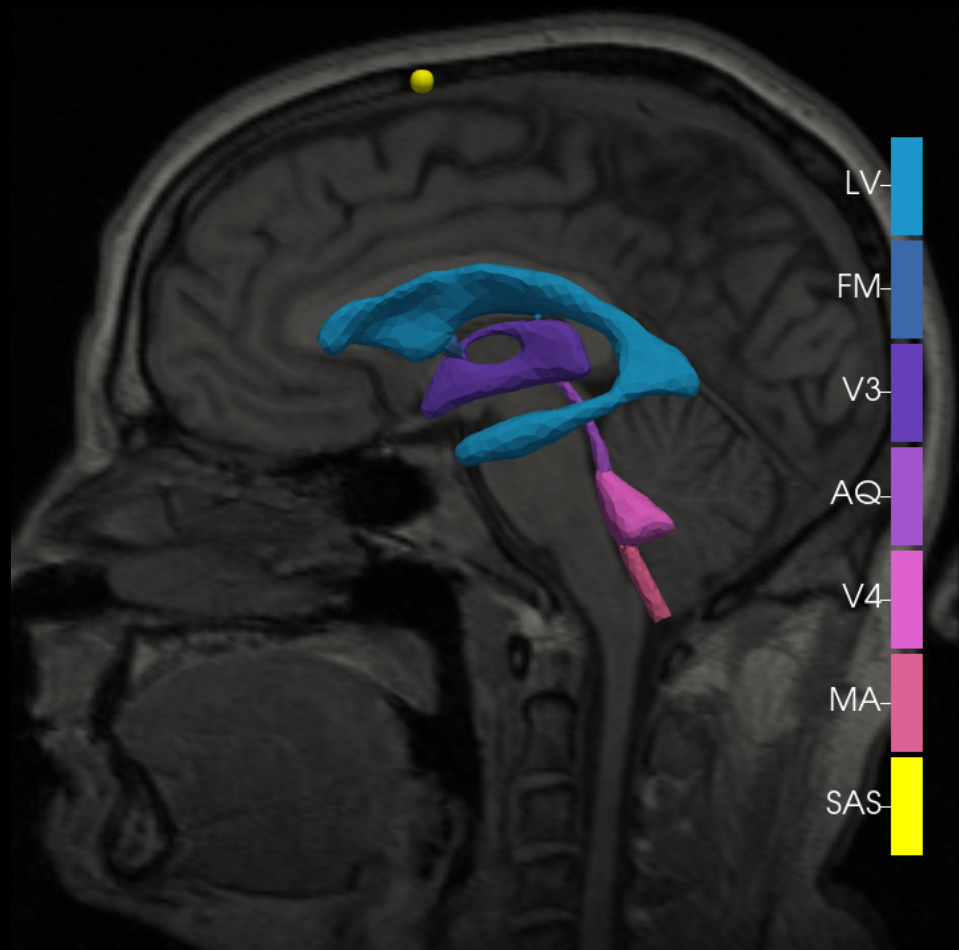
(III) brain equilibrium phase

(IV) high net outflow of blood



varying in time, spatially  
uniform mass source term  $g$

# The model is based on a detailed, MRI-derived geometry



# The fluid-poroelastic coupling is based on first principles

**Mass conservation on  $\Sigma$**

$$\mathbf{u} \cdot \mathbf{n} = \left( \partial_t \mathbf{d} + \frac{\kappa}{\mu_F} \nabla p_P \right) \cdot \mathbf{n}$$

**Momentum conservation on  $\Sigma$**

$$(2\mu_F \epsilon(\mathbf{u}) - p_F \mathbf{I}) \mathbf{n} = (2\mu_S \epsilon(\mathbf{d}) - \phi \mathbf{I}) \mathbf{n}$$

**Balance of total normal stress on  $\Sigma$**

$$p_p + \mathbf{n} \cdot (2\mu_F \epsilon(\mathbf{u}) - p_F \mathbf{I}) \mathbf{n} = 0$$

**Beavers-Joseph-Saffman condition on  $\Sigma$**

$$-\mathbf{n} \cdot (2\mu_F \epsilon(\mathbf{u}) - p_F \mathbf{I}) \tau_i = \frac{\gamma \mu_F}{\sqrt{\kappa}} (\mathbf{u} - \partial_t \mathbf{d}) \cdot \tau_i$$

with the tangential vectors  $\tau_i, i = 1, 2$

# The boundary conditions represent a rigid skull and a compliant spinal compartment

**Rigid skull**

$$\mathbf{u} = 0 \quad \text{on } \Gamma_{\text{skull}}$$

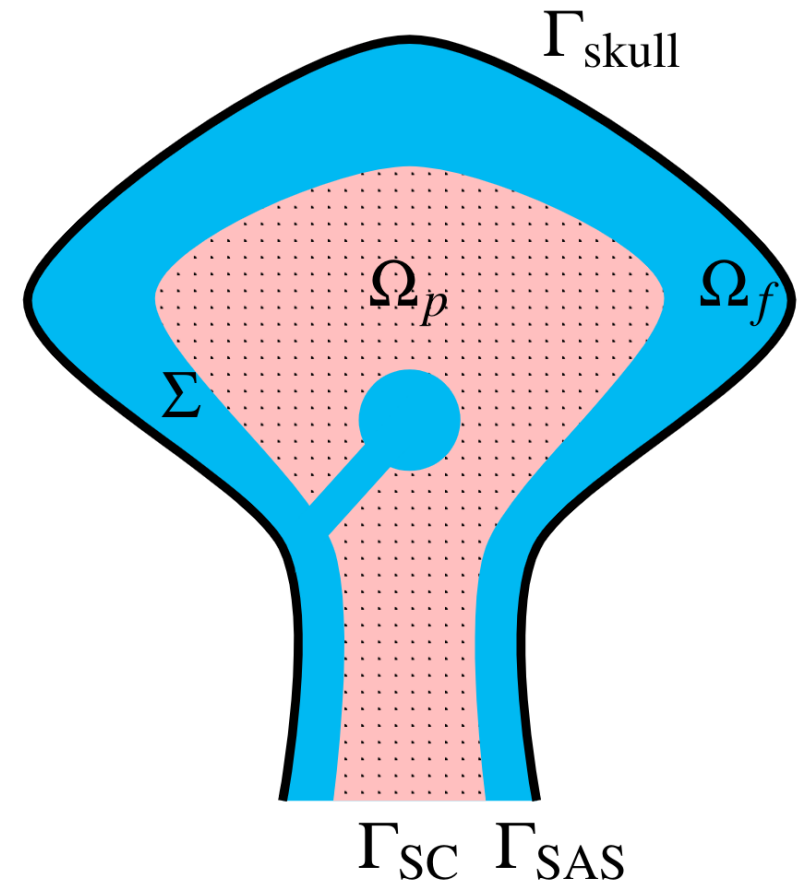
**Spinal coord**

$$\mathbf{d} = 0 \quad \text{and} \quad \frac{\kappa}{\mu_f} \nabla p_p \cdot \mathbf{n} = 0 \quad \text{on } \Gamma_{\text{SC}}$$

**Spinal SAS**

$$(2\mu_f \epsilon(\mathbf{u}) - p_f \mathbf{I}) \cdot \mathbf{n} = -\mathbf{n} p_0 \cdot 10^{\Delta V_{\text{out}}(t)/PVI_{\text{SC}}} \quad \text{on } \Gamma_{\text{SAS}}$$

$$\text{with } \Delta V_{\text{out}}(t) = \int_0^t \int_{\Gamma_{\text{SAS}}} \mathbf{u} \cdot \mathbf{n} \, ds \, dt$$





# The model is solved using a monolithic finite element approach

- total pressure formulation for Biot
- Taylor-Hood type elements (P2-P1-P2-P1-P1)
- implicit Euler time discretization

## Block System

At each time step, find  $\mathbf{u}_h^{n+1}$ ,  $p_{F,h}^{n+1}$ ,  $\mathbf{d}_h^{n+1}$ ,  $p_{P,h}^{n+1}$  and  $\phi$  such that

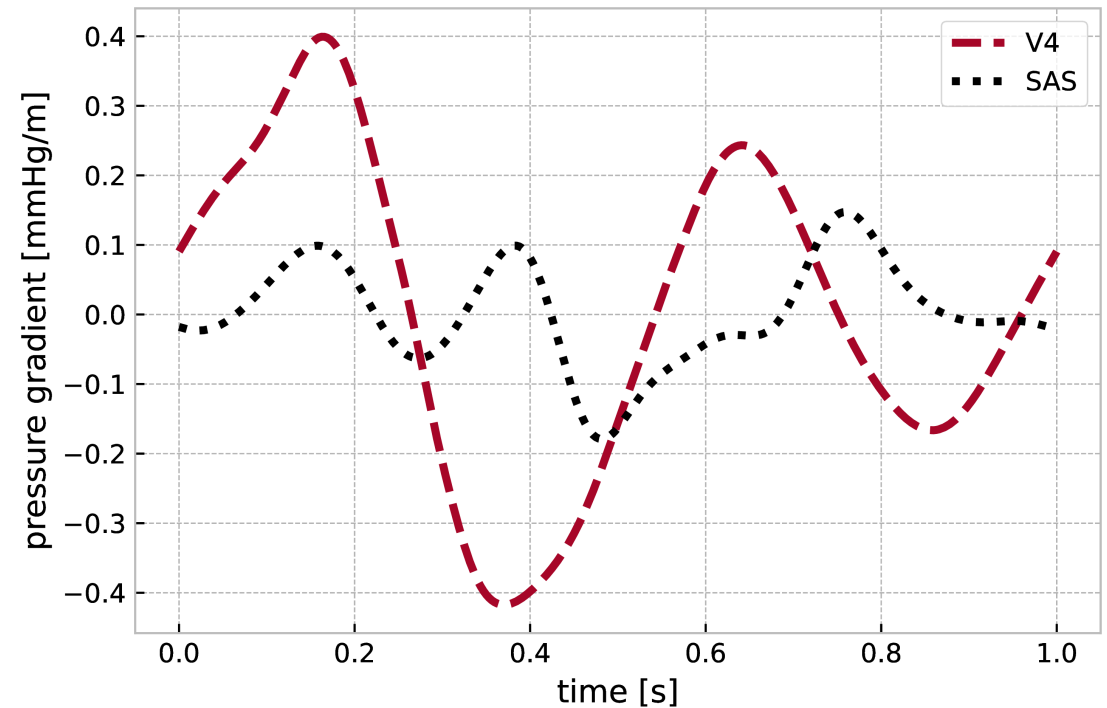
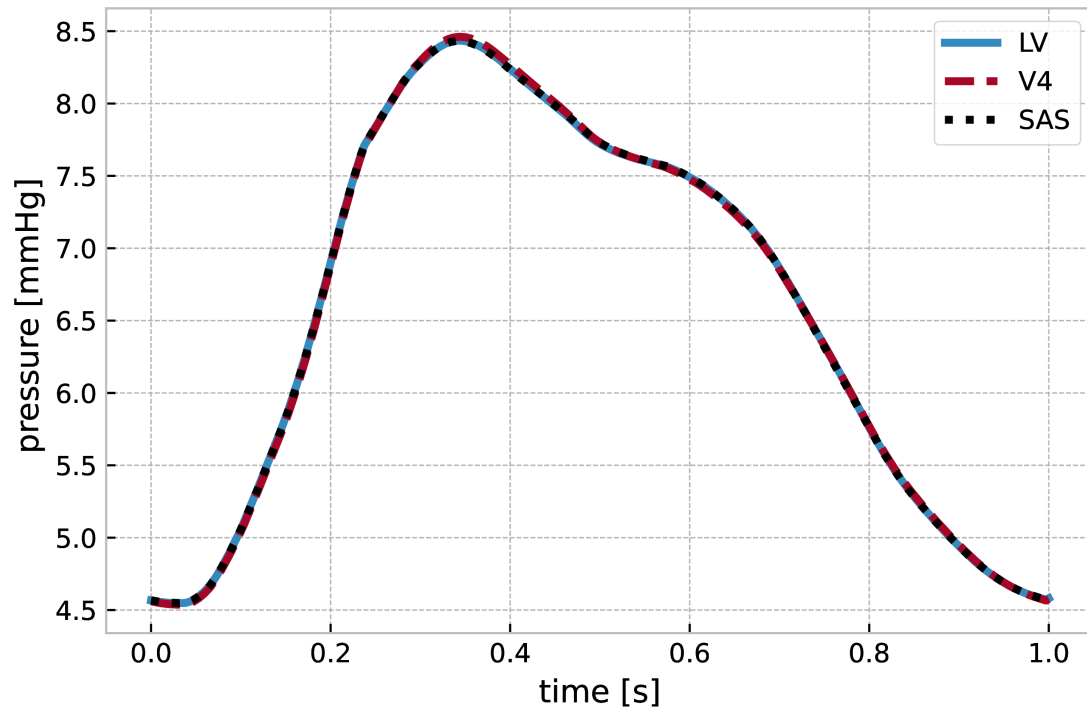
$$\begin{bmatrix} \mathcal{A}^F & (\mathcal{B}_1^F)' & \frac{1}{\Delta t} (\mathcal{B}_3^\Sigma)' & (\mathcal{B}_2^\Sigma)' & 0 \\ \mathcal{B}_1^F & 0 & 0 & 0 & 0 \\ \mathcal{B}_3^\Sigma & 0 & \mathcal{A}_1^P & (\mathcal{B}_4^\Sigma)' & (\mathcal{B}_1^P)' \\ -\mathcal{B}_2^\Sigma & 0 & -\frac{1}{\Delta t} \mathcal{B}_4^\Sigma & \mathcal{A}_2^P & -\frac{1}{\Delta t} (\mathcal{B}_2^P)' \\ 0 & 0 & \mathcal{B}_1^P & \mathcal{B}_2^P & -\mathcal{A}_3^P \end{bmatrix} \begin{bmatrix} \mathbf{u}_h^{n+1} \\ p_{F,h}^{n+1} \\ \mathbf{d}_h^{n+1} \\ p_{P,h}^{n+1} \\ \phi_h^{n+1} \end{bmatrix} = \begin{bmatrix} \mathcal{F}^{F,n} \\ 0 \\ \mathcal{F}^{P,n} \\ \mathcal{G}^n \\ 0 \end{bmatrix}$$

## Implementation

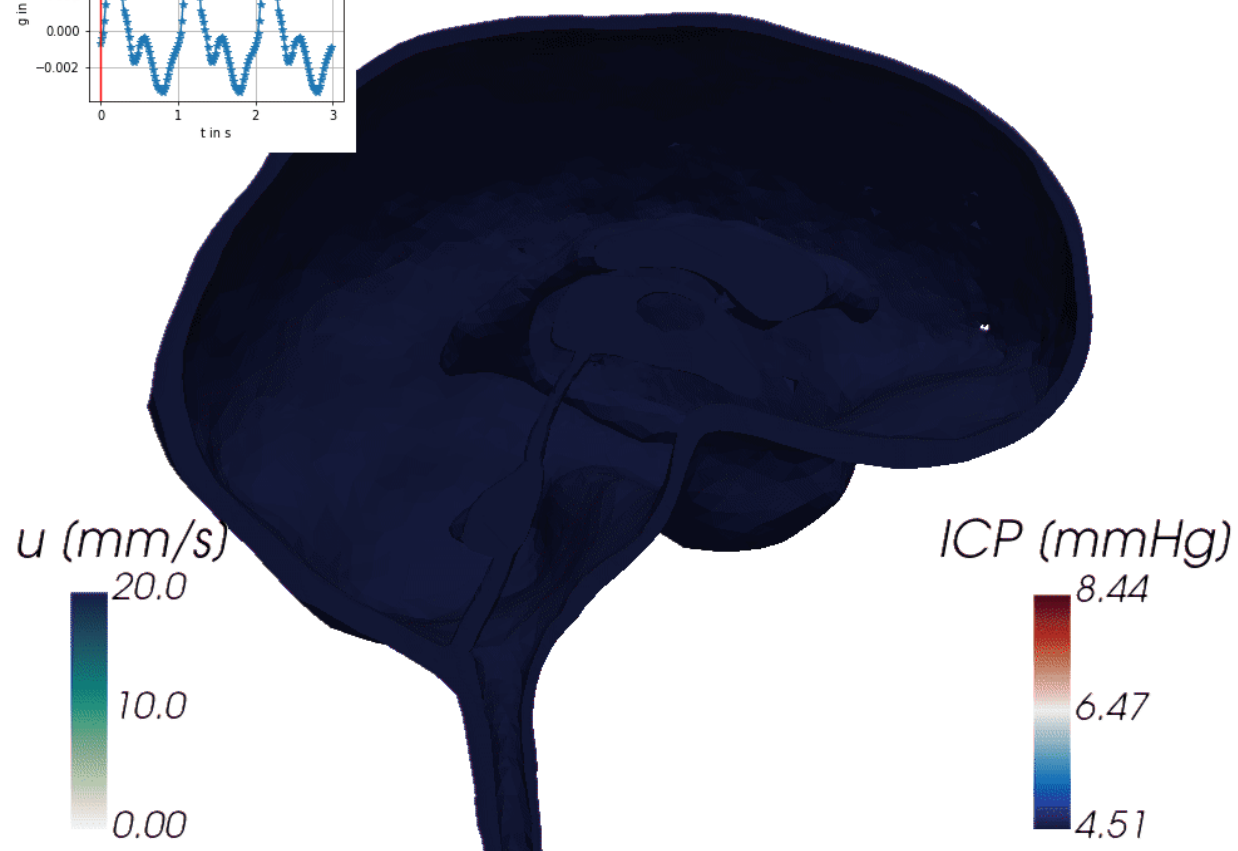
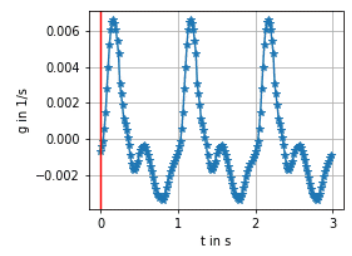
- direct solver (MUMPS)
- implementation based on Fenics & Multiphenics



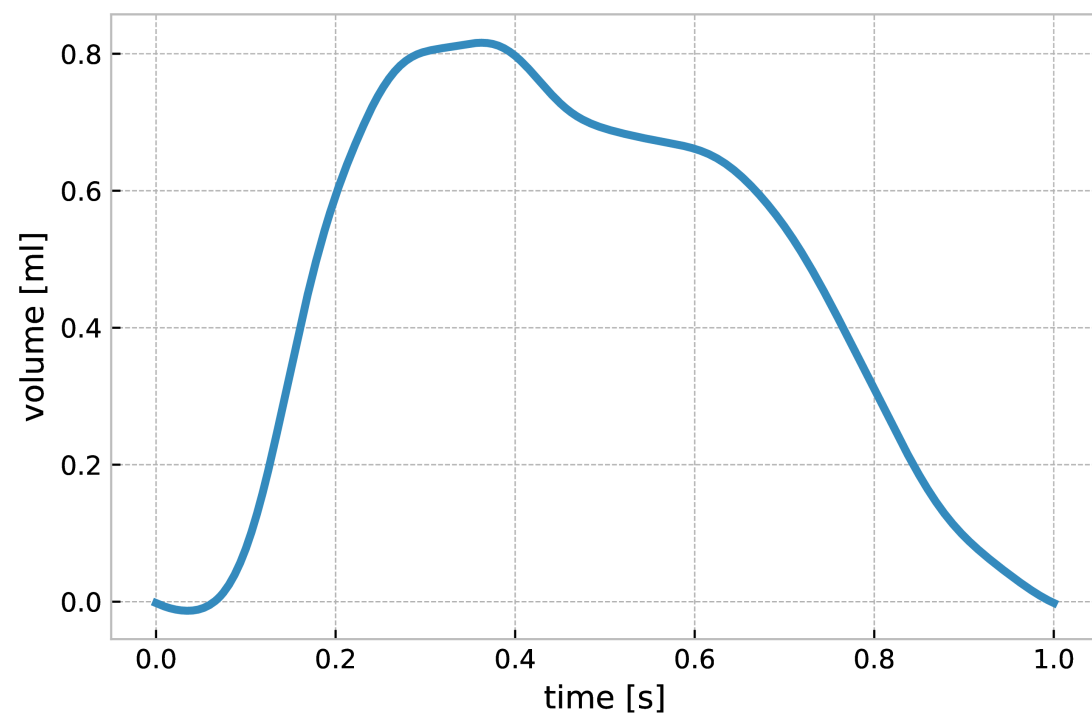
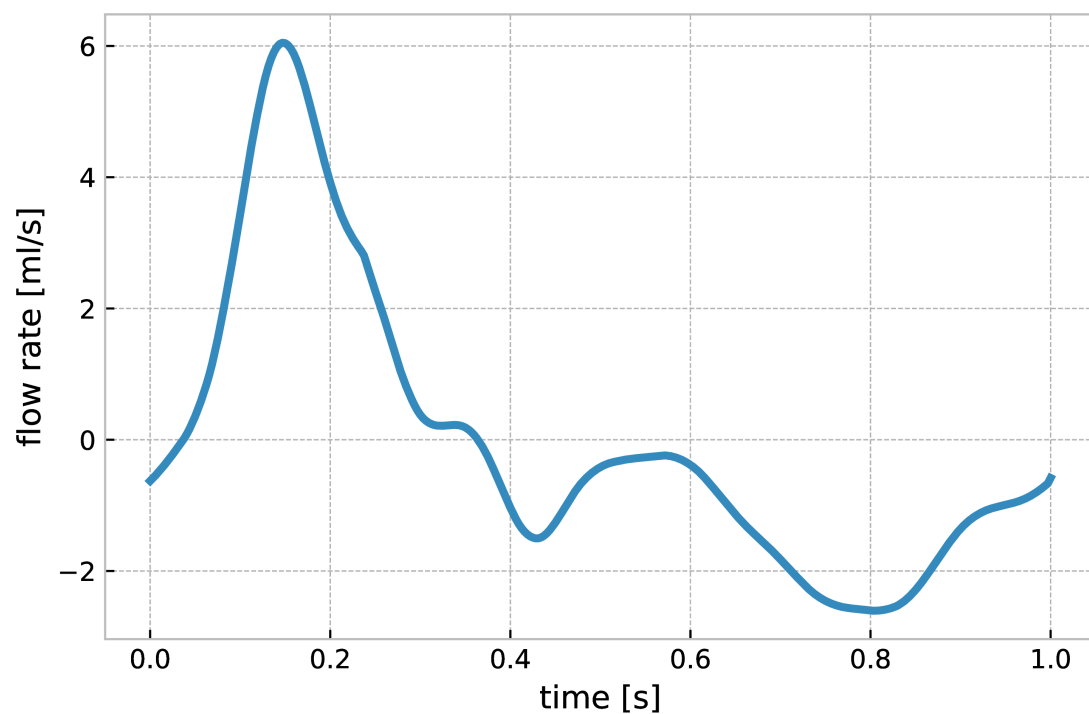
# Variations in the ICP are dominated by their temporal amplitude



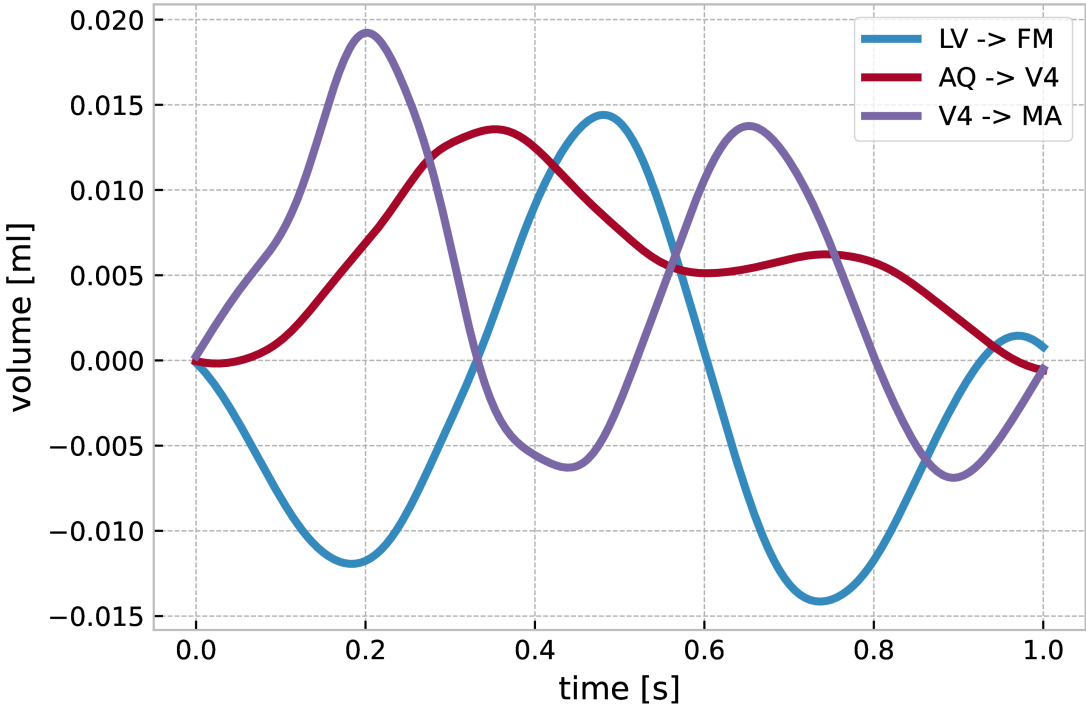
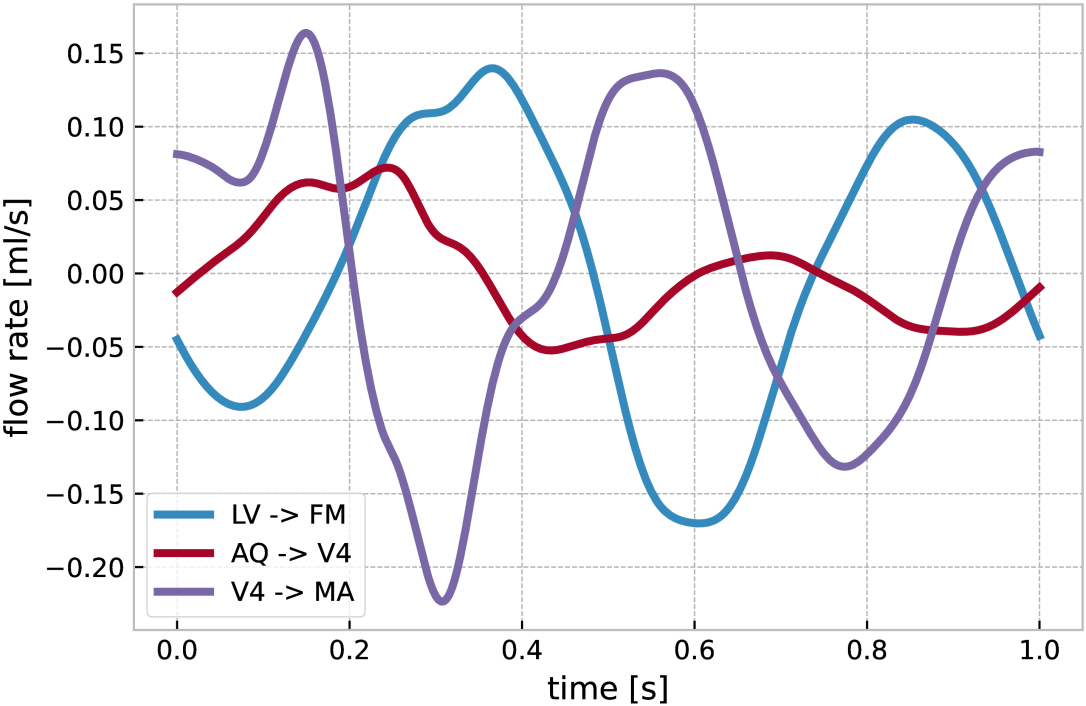
# Cardiac pulsations cause substantial pressure variations and complex flow patterns



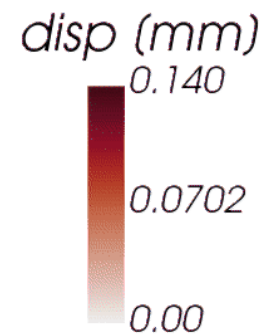
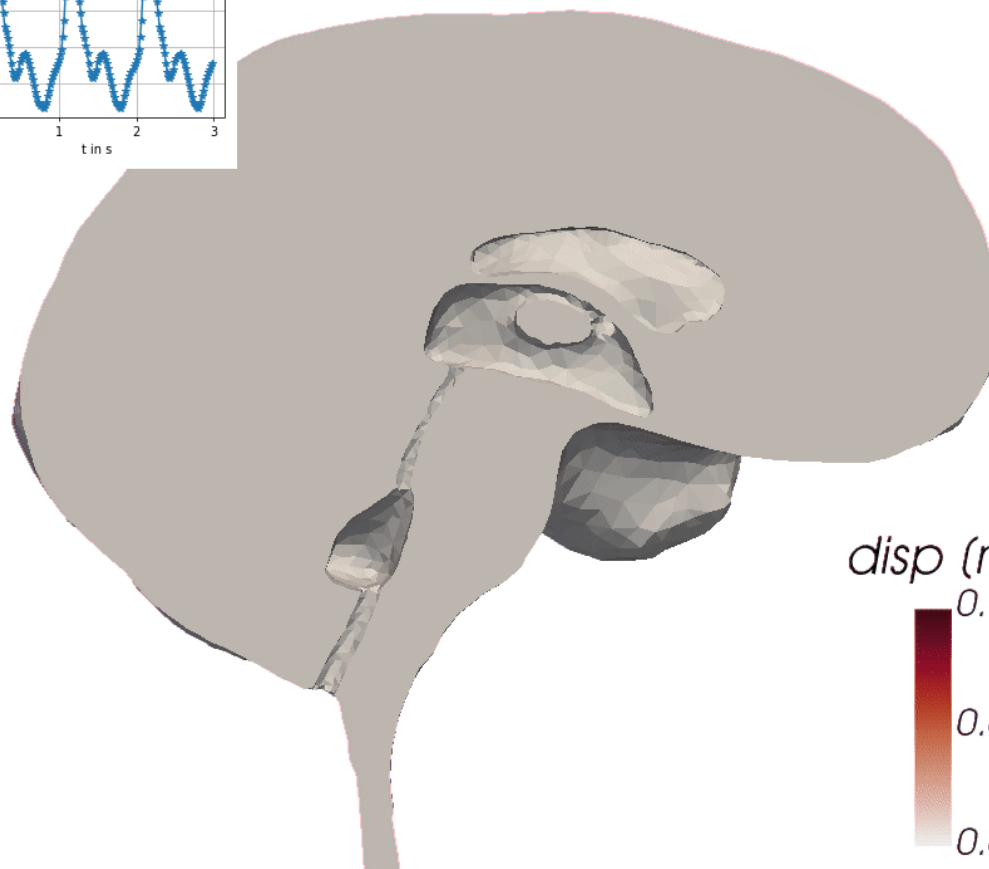
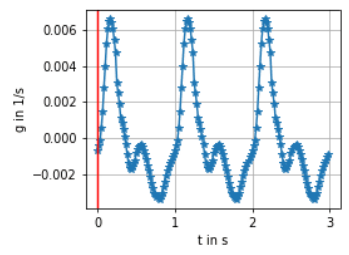
# The largest peak flow rates occur into the spinal canal



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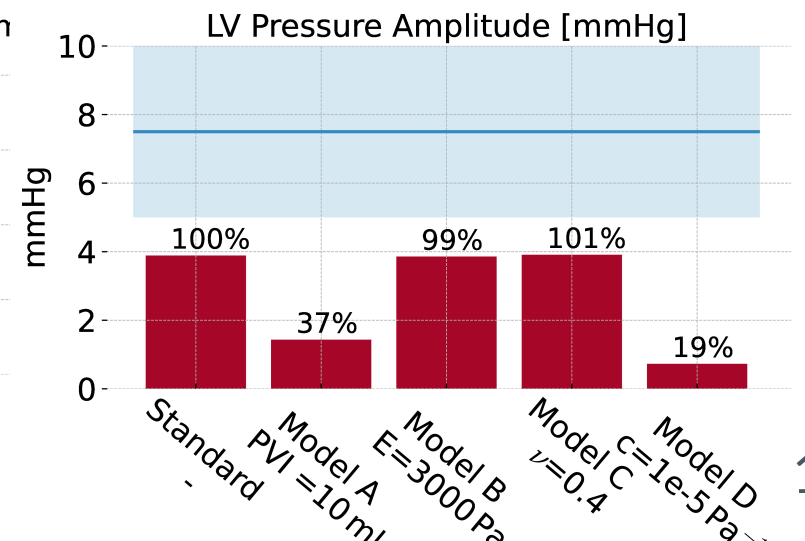
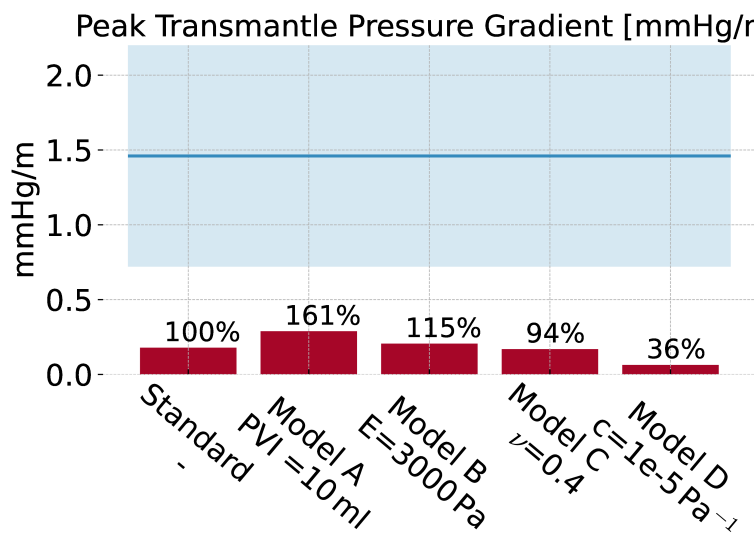
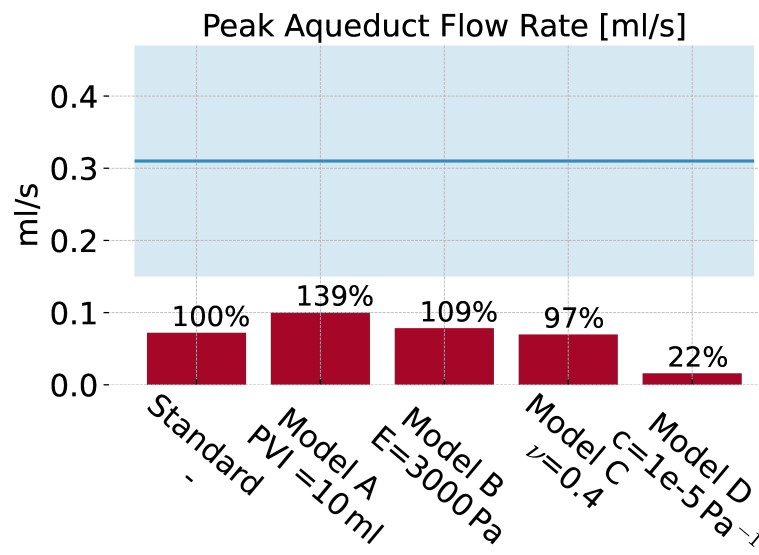
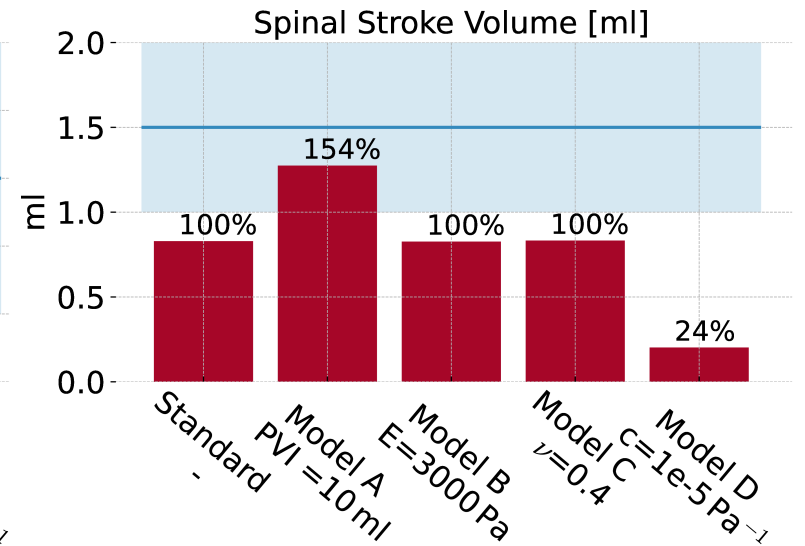
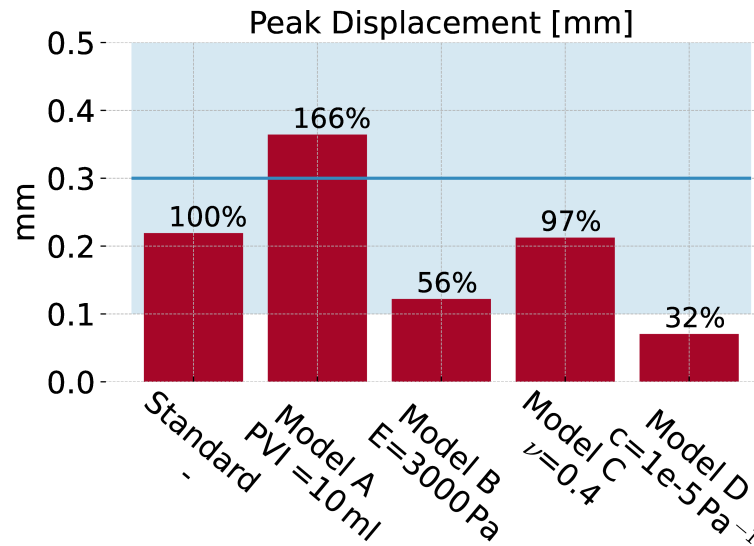
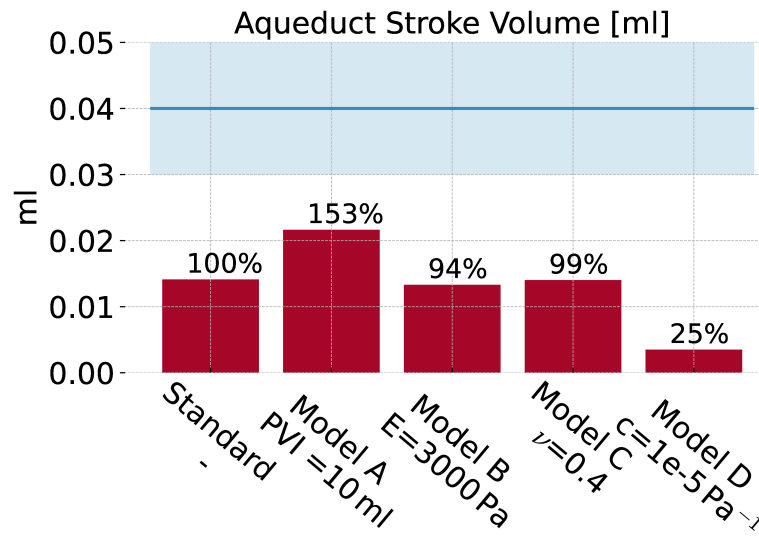
# The brain tissue rotates and exhibits a funnel-shaped motion at the brain stem



# We compute the effect of a selection of parameter deviations

Model	modified parameter	value	interpretation
Standard	-	-	-
A	pressure-volume index	$PVI = 10 \text{ ml}$	greater spinal compliance
B	Young Modulus	$E = 3000 \text{ Pa}$	stiffer brain parenchyma
C	Poisson ratio	$\nu = 0.4$	greater compressibility of parenchymal tissue
D	storage coefficient	$c = 10^{-5} \text{ Pa}^{-1}$	greater cranial compliance

# Model variations



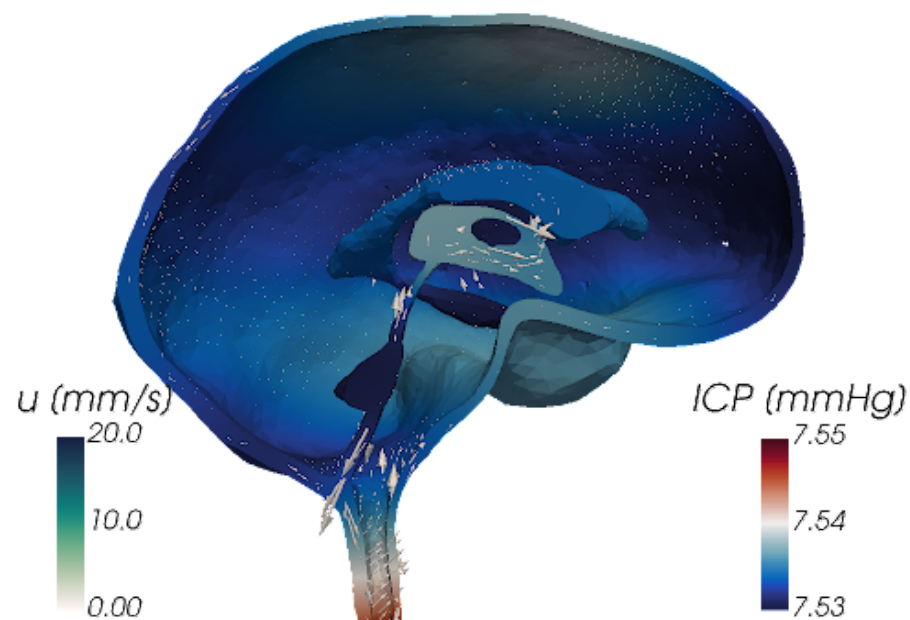


# In conclusion, we present a new computational framework of cardiac-induced intracranial motion

our model predicts ICP, CSF flow and tissue displacement with high resolution in space and time



new insights into intracranial pulsatility in health and disease



simula



Causemann, M., Vinje, V., & Rognes, M. E. (2022). *Human intracranial pulsatility during the cardiac cycle: a computational modelling framework*, biorxiv